

**Project:** Steel to concrete connection  
**Project no:**  
**Author:**

## Project data

Project name	Steel to concrete connection
Project number	
Author	
Description	
Date	4/10/2025
Code	AISC/ACI

## Material

Steel	A992, A572 Gr.50, A500. Gr. C, A572 Gr.50, A572 Gr.50
Concrete	4000 psi

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## Project item Base plate connection

### Design

Name Base plate connection  
 Description  
 Analysis Stress, strain/ loads in equilibrium  
 Design code AISC 360-22 (LRFD) / ACI 318-19

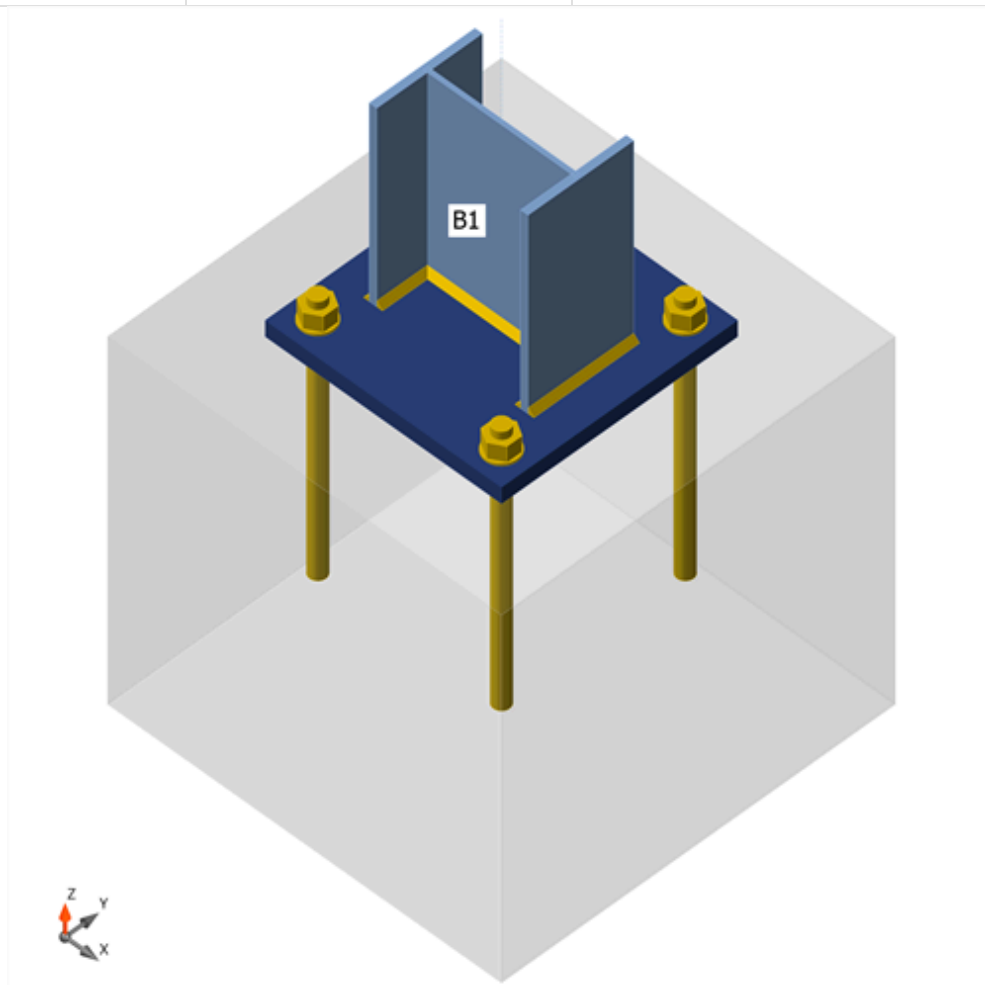
### Members

#### Geometry

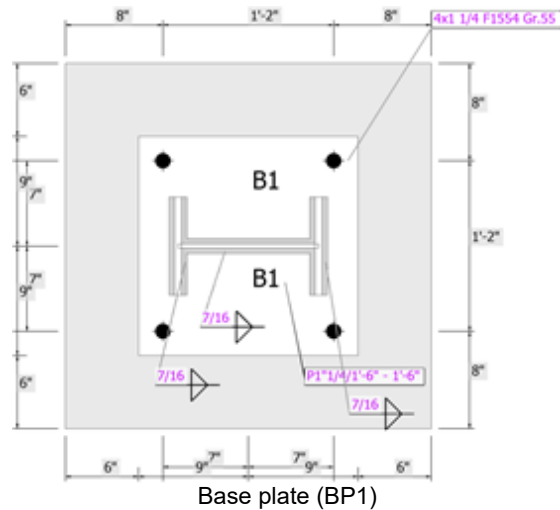
Name	Cross-section	$\beta$ - Direction [°]	$\gamma$ - Pitch [°]	$\alpha$ - Rotation [°]	Offset ex [in]	Offset ey [in]	Offset ez [in]
B1	2 - W12X45	0.0	90.0	0.0	0"	0"	0"

#### Supports and forces

Name	Support	Forces in	X [in]
B1 / end		Node	0"



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## Cross-sections

Name	Material
2 - W12X45	A992

## Anchors

Name	Diameter [in]	$f_y$ [ksi]	$f_u$ [ksi]	Gross area [in <sup>2</sup> ]
1 1/4 F1554 Gr.55	1 1/4	55.0	75.0	1.2272

## Load effects (forces in equilibrium)

Name	Member	N [kip]	V <sub>y</sub> [kip]	V <sub>z</sub> [kip]	M <sub>x</sub> [kip.ft]	M <sub>y</sub> [kip.ft]	M <sub>z</sub> [kip.ft]
N+V <sub>z</sub> +M <sub>y</sub>	B1 / End	17.00	0.00	10.00	0.00	60.00	0.00
Uplift+V <sub>z</sub>	B1 / End	80.00	0.00	20.00	0.00	0.00	0.00
Uplift+V <sub>y</sub>	B1 / End	80.00	20.00	0.00	0.00	0.00	0.00

## Unbalanced forces

Name	X [kip]	Y [kip]	Z [kip]	M <sub>x</sub> [kip.ft]	M <sub>y</sub> [kip.ft]	M <sub>z</sub> [kip.ft]
N+V <sub>z</sub> +M <sub>y</sub>	-10.00	0.00	17.00	0.00	60.00	0.00
Uplift+V <sub>z</sub>	-20.00	0.00	80.00	0.00	0.00	0.00
Uplift+V <sub>y</sub>	0.00	20.00	80.00	0.00	0.00	0.00

## Foundation block

Item	Value	Unit
<b>CB 1</b>		
Dimensions	2'-6" x 2'-6"	in
Depth	2'-4"	in
Anchor	1 1/4 F1554 Gr.55	
Anchoring length	1'-6"	in
Shear force transfer	Anchors	

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## Check

### Summary

Name	Value	Check status
Analysis	100.0%	OK
Plates	0.0 < 5.0%	OK
Anchors	62.8 < 100%	OK
Welds	80.8 < 100%	OK
Concrete block	14.6 < 100%	OK
Buckling	Not calculated	

### Plates

Name	Material	t <sub>p</sub> [in]	Loads	σ <sub>Ed</sub> [ksi]	ε <sub>pI</sub> [%]	σ <sub>c,Ed</sub> [ksi]	Status
B1-bfl 1	A992	9/16	Uplift+Vy	34.9	0.0	0.0	OK
B1-tfl 1	A992	9/16	N+Vz+My	39.8	0.0	0.0	OK
B1-w 1	A992	5/16	Uplift+Vz	16.7	0.0	0.0	OK
BP1	A572 Gr.50	1"1/4	N+Vz+My	43.6	0.0	0.0	OK

### Design data

Material	F <sub>y</sub> [ksi]	ε <sub>lim</sub> [%]
A992	50.0	5.0
A572 Gr.50	50.0	5.0

### Detailed result for B1-tfl 1

#### Design values used in the analysis

$$\phi F_y = 45.0 \text{ ksi}$$

Where:

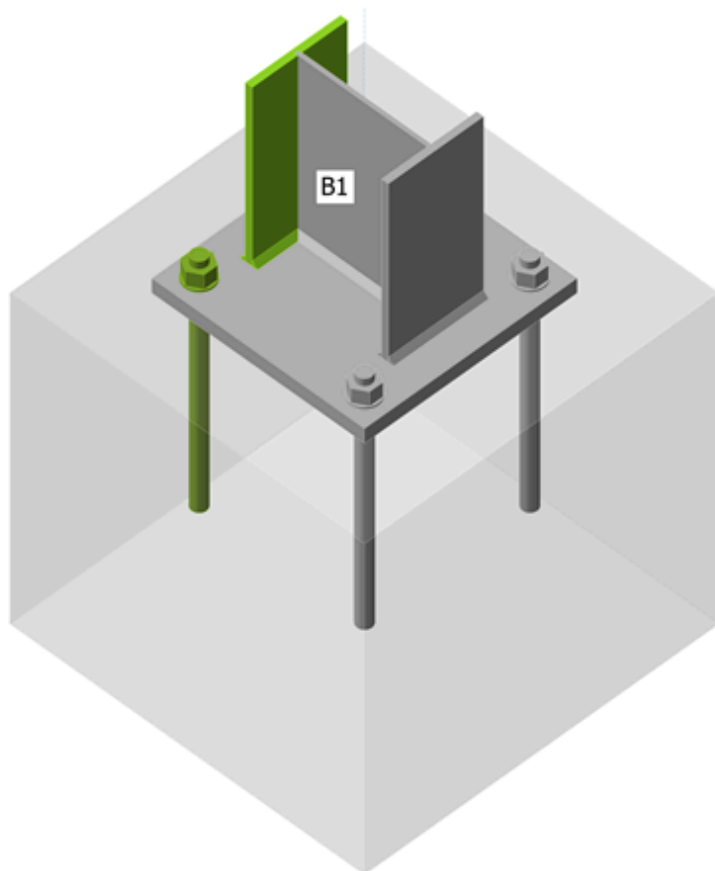
$F_y = 50.0 \text{ ksi}$  – characteristic yield strength

$\phi = 0.90$  – resistance factor for steel material AISC 360-22 – B3.1

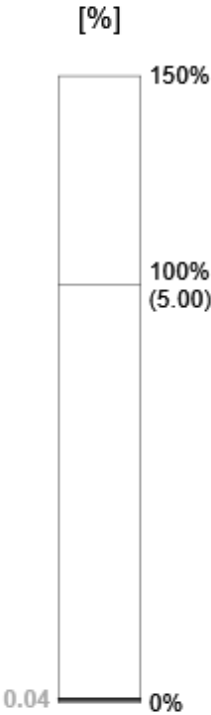
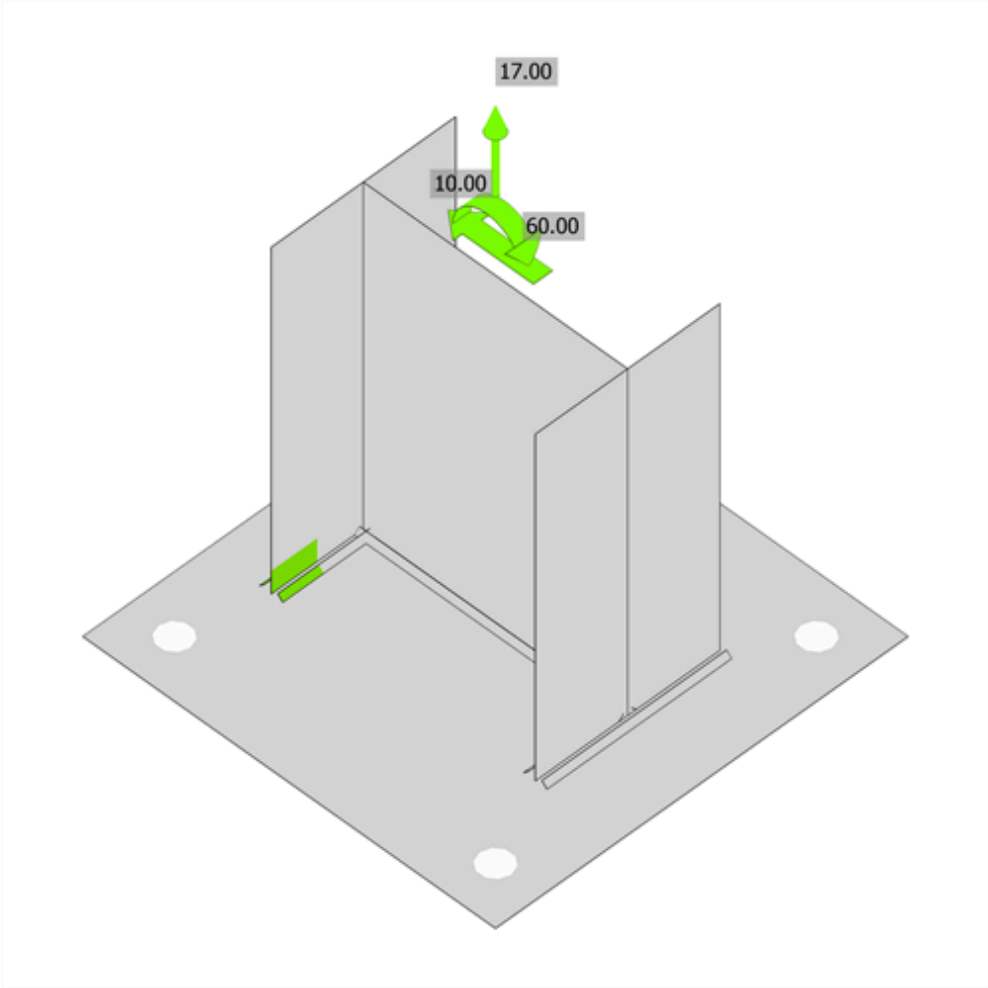
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*Overall check,  $N+V_z+M_y$*

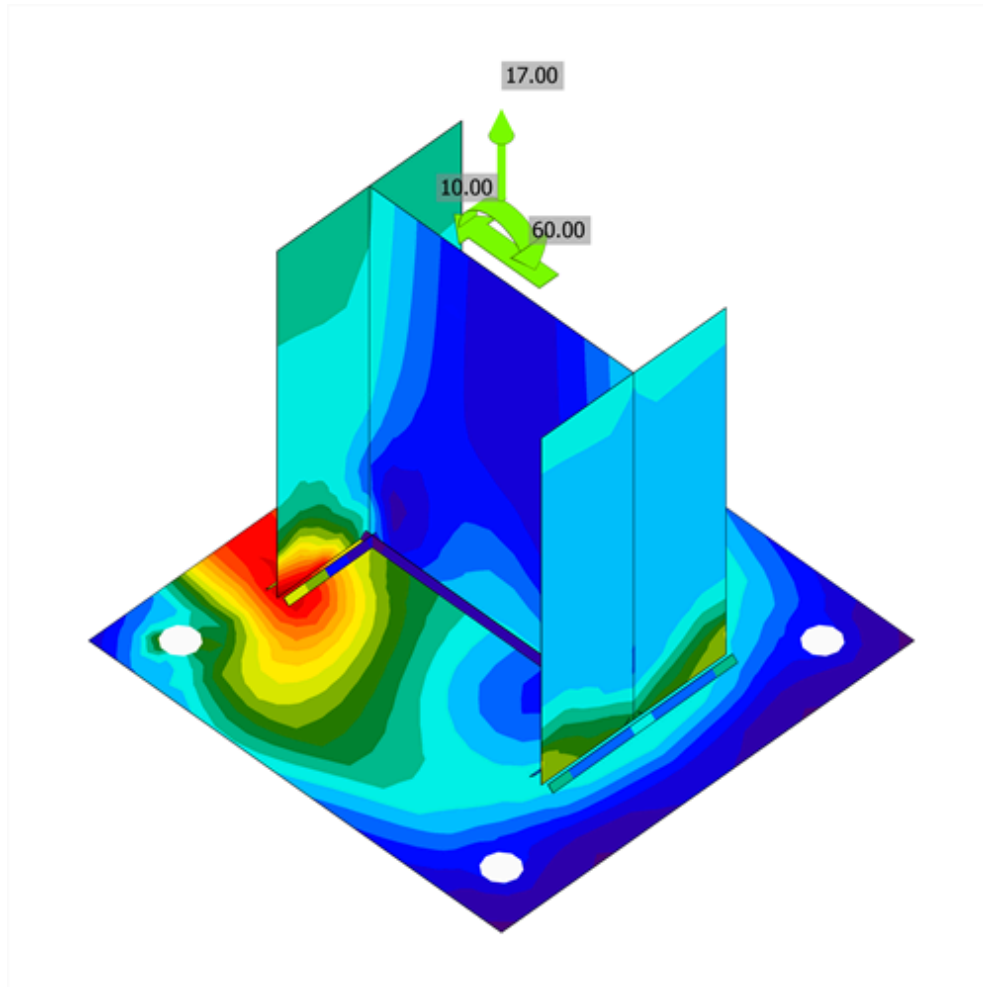


Strain check,  $N+Vz+My$

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Equivalent stress,  $N+Vz+My$

## Anchors

Shape	Item	Loads	$N_f$ [kip]	$V$ [kip]	$U_{t_t}$ [%]	$U_{t_s}$ [%]	$U_{t_{ts}}$ [%]	Detailing	Status
	A1	Uplift+Vy	22.15	4.71	43.5	16.6	30.0	OK	OK
	A2	$N+Vz+My$	31.93	2.55	62.8	9.0	47.8	OK	OK
	A3	Uplift+Vz	22.11	5.01	43.5	17.7	30.5	OK	OK
	A4	$N+Vz+My$	31.94	2.55	62.8	9.0	47.8	OK	OK

## Design data

Grade	$\phi N_{sa}$ [kip]	$\phi V_{sa}$ [kip]
1 1/4 F1554 Gr.55 - 1	50.87	28.34

## Detailed result for A4

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Following checks of anchors loaded in tension are not provided and should be checked using information in relevant Technical Product Specification (based on the 5 percent fractile of tests performed and evaluated according to ACI 355.2):

- Pull-out failure of fastener (for post-installed mechanical anchors) - ACI 318-19 – 17.6.3
- Bond strength of adhesive anchor (for post-installed bonded anchors) - ACI 318-19 – 17.6.5
- Concrete splitting failure during installation should be evaluated by ACI 355.2 requirements

Concrete blow-out failure is provided only for anchors with washer plates.

**Anchor tensile resistance** (ACI 318-19 – 17.6.1)

$$\phi N_{sa} = \phi \cdot A_{se,N} \cdot f_{uta} = 50.87 \text{ kip} \geq N_f = 31.94 \text{ kip}$$

Where:

$\phi = 0.70$  – resistance factor

$A_{se,N} = 0.9690 \text{ in}^2$  – tensile stress area

$f_{uta} = 75.0 \text{ ksi}$  – specified tensile strength of anchor steel:

- $f_{uta} = \min(125 \text{ ksi}, 1.9 \cdot f_{ya}, f_u)$  , where:
  - $f_{ya} = 55.0 \text{ ksi}$  – specified yield strength of anchor steel
  - $f_u = 75.0 \text{ ksi}$  – specified ultimate strength of anchor steel

**Shear resistance** (ACI 318-19 – 17.7.1)

$$\phi V_{sa} = \phi \cdot 0.6 \cdot A_{se,V} \cdot f_{uta} = 28.34 \text{ kip} \geq V = 2.55 \text{ kip}$$

Where:

$\phi = 0.65$  – resistance factor

$A_{se,V} = 0.9690 \text{ in}^2$  – tensile stress area

$f_{uta} = 75.0 \text{ ksi}$  – specified tensile strength of anchor steel:

- $f_{uta} = \min(125 \text{ ksi}, 1.9 \cdot f_{ya}, f_u)$  , where:
  - $f_{ya} = 55.0 \text{ ksi}$  – specified yield strength of anchor steel
  - $f_u = 75.0 \text{ ksi}$  – specified ultimate strength of anchor steel

**Interaction of tensile and shear forces** (ACI 318-19 – R17.8)

$$U_{tt}^{5/3} + U_{ts}^{5/3} = 0.48 \leq 1.0$$

Where:

$U_{tt} = 0.63$  – maximum ratio of factored tensile force and tensile resistance determined from all appropriate failure modes

$U_{ts} = 0.09$  – maximum ratio of factored shear force and shear resistance determined from all appropriate failure modes

**Supplementary reinforcement** (ACI 318-19 – 17.5.2.1 ; ACI 318-19 – 17.5.2.1 )

Supplementary reinforcement should resist force of 63.87 kip in tension and 10.00 kip in shear. Only current load effect considered.



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## Welds

Item	Edge	Xu	t <sub>w</sub> [in]	w [in]	L [in]	L <sub>c</sub> [in]	Loads	F <sub>n</sub> [kip]	φR <sub>n</sub> [kip]	Ut [%]	Ut <sub>c</sub> [%]	Detailing	Status
BP1	B1-bfl 1	E70xx	▲ 5/16 ▼	▲ 7/16 ▼	8"1/16	7/8	Uplift+Vy	9.14	11.85	77.2	60.9	OK	OK
		E70xx	▲ 5/16 ▼	▲ 7/16 ▼	8"1/16	7/8	Uplift+Vy	9.19	11.85	77.5	63.0	OK	OK
BP1	B1-tfl 1	E70xx	▲ 5/16 ▼	▲ 7/16 ▼	8"1/16	7/8	N+Vz+My	9.96	12.33	80.8	72.5	OK	OK
		E70xx	▲ 5/16 ▼	▲ 7/16 ▼	8"1/16	7/8	N+Vz+My	9.79	12.27	79.8	72.1	OK	OK
BP1	B1-w 1	E70xx	▲ 5/16 ▼	▲ 7/16 ▼	11"1/2	7/8	Uplift+Vz	1.35	9.98	13.5	5.4	OK	OK
		E70xx	▲ 5/16 ▼	▲ 7/16 ▼	11"1/2	7/8	Uplift+Vz	1.39	9.95	14.0	5.6	OK	OK

## Design data

Material	F <sub>exx</sub> [ksi]
E70xx	70.0

## Detailed result for BP1 / B1-tfl 1

### Weld resistance check (AISC 360-22 – J2-4)

$$\phi R_n = \phi \cdot F_{nw} \cdot A_{we} = 12.33 \text{ kip} \geq F_n = 9.96 \text{ kip}$$

Where:

$F_{nw} = 58.9 \text{ ksi}$  – nominal stress of weld material:

- $F_{nw} = 0.6 \cdot F_{EXX} \cdot (1 + 0.5 \cdot \sin^{1.5} \theta)$ , where:
  - $F_{EXX} = 70.0 \text{ ksi}$  – electrode classification number, i.e. minimum specified tensile strength
  - $\theta = 60.1^\circ$  – angle of loading measured from the weld longitudinal axis

$A_{we} = 0.2789 \text{ in}^2$  – effective area of weld critical element

$\phi = 0.75$  – resistance factor for welded connections

## Concrete block

Item	Loads	A <sub>1</sub> [in <sup>2</sup> ]	A <sub>2</sub> [in <sup>2</sup> ]	σ [ksi]	φf <sub>p,max</sub> [ksi]	Ut [%]	Status
CB 1	Uplift+Vz	14.8867	716.0784	0.6	4.4	14.6	OK

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### Detailed result for CB 1

#### Concrete block compressive resistance check (AISC 360-22 – J8)

$$\phi_c f_{p,max} = 4.4 \text{ ksi} \geq \sigma = 0.6 \text{ ksi}$$

Where:

$f_{p,max} = 6.8 \text{ ksi}$  – concrete block design bearing strength:

- $f_{p,max} = 0.85 \cdot f'_c \cdot \sqrt{\frac{A_2}{A_1}} \leq 1.7 \cdot f'_c$ , where:
  - $f'_c = 4.0 \text{ ksi}$  – concrete compressive strength
  - $A_1 = 14.8867 \text{ in}^2$  – base plate area in contact with concrete surface
  - $A_2 = 716.0784 \text{ in}^2$  – concrete supporting surface


$\phi_c = 0.65$  – resistance factor for concrete

### Buckling

Buckling analysis was not calculated.

## Bill of material

### Manufacturing operations

Name	Plates [in]	Shape	Nr.	Welds [in]	Length [in]	Bolts	Nr.
BP1	P1"1/4x1'-6"-1'-6" (A572 Gr.50)		1	Double fillet: 7/16	2'-3"5/8	1 1/4 F1554 Gr.55	4

### Symbol explanation

Fillet weld

leg size of weld

### Welds

Type	Material	Throat thickness [in]	Leg size [in]	Length [in]
Double fillet	E70xx	5/16	7/16	2'-3"5/8

### Anchors

Name	Length [in]	Drill length [in]	Count
1 1/4 F1554 Gr.55	1'-7"1/4	1'-6"	4

### Drawing

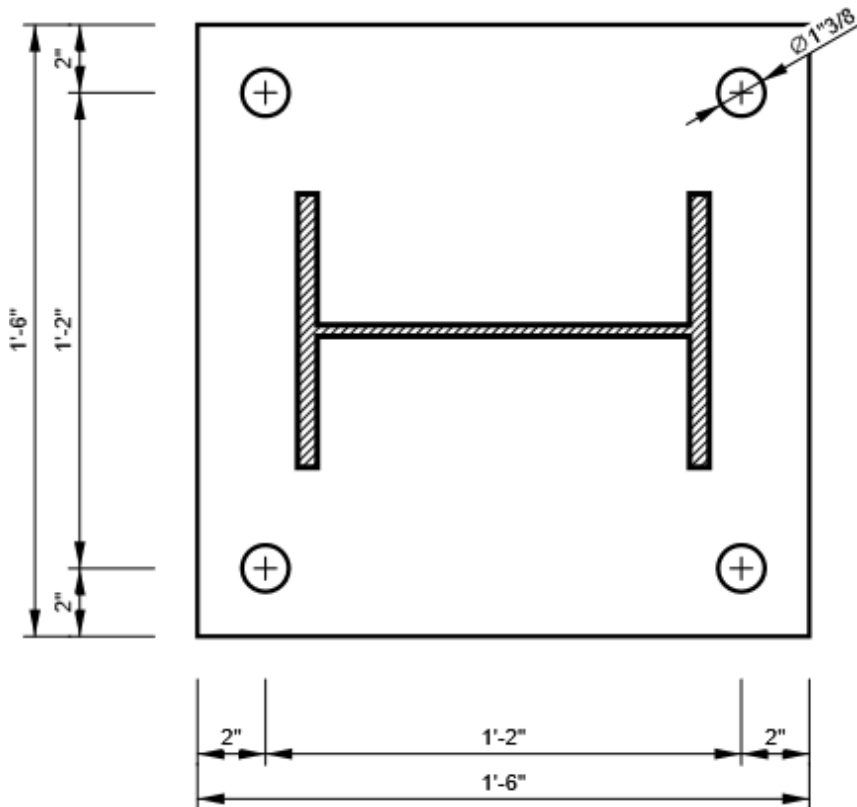
BP1

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P1"1/4x1'-6"-1'-6" (A572 Gr.50)



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## Symbol explanation

Symbol	Explanation
$t_p$	Plate thickness
$\sigma_{Ed}$	Equivalent stress
$\varepsilon_{pl}$	Plastic strain
$\sigma_{c,Ed}$	Contact stress
$F_y$	Yield strength
$\varepsilon_{lim}$	Limit of plastic strain
$N_f$	Tension force
$V$	Resultant of bolt shear forces $V_y$ and $V_z$ in shear planes
$U_{t_t}$	Utilization in tension
$U_{t_s}$	Utilization in shear
$U_{t_{ts}}$	Utilization in tension and shear
$\phi N_{sa}$	Steel strength of anchor in tension - ACI 318-19 – 17.6.1
$\phi V_{sa}$	Steel strength of anchor in shear - ACI 318-19 – 17.7.1
$t_w$	Throat thickness of weld
$w$	Leg size of weld
$L$	Length of weld
$L_c$	Length of weld critical element
$F_n$	Force in weld critical element
$\phi R_n$	Weld resistance - AISC 360-22 – J2-4
$U_t$	Utilization
$U_{t_c}$	Weld capacity estimation
	Fillet weld
$F_{exx}$	Ultimate strength as rated by electrode classification number
$A_1$	Loaded area
$A_2$	Supporting area
$\sigma$	Average stress in concrete
$\phi f_{p,max}$	Concrete bearing resistance

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## Code settings

Item	Value	Unit	Reference
Friction coefficient - concrete	0.40	-	ACI 349-01 – B.6.1.4
Friction coefficient in slip-resistance	0.30	-	AISC 360-22 – J3.9
Limit plastic strain	0.05	-	
Detailing	Yes		
Distance between bolts [d]	2.66	-	AISC 360-22 – J3.4
Concrete breakout resistance check	None		
Base metal capacity check at weld fusion face	No		AISC 360-22 – J2-2
Deformation at bolt hole at service load is design consideration	Yes		AISC 360-22 – J3.11
Cracked concrete	Yes		ACI 318-19 – 17
Local deformation check	Yes		
Local deformation limit	0.03	-	CIDECT DG 1, 3 – 1.1
Geometrical nonlinearity (GMNA)	Yes		Analysis with large deformations for hollow section joints

## Software info

Application                      IDEA StatiCa Connection  
Version                            25.0.0.2048  
Developed by                    IDEA StatiCa